

Homework #1 Solutions

1. (10 pts) Assuming air density is a *constant* 1.23 kg/m^3 , calculate the change of air pressure from the top of a mountain to its base if the elevation is 3000 meters. Give your answer in kPa .

Solution: Calculate directly from the hydrostatic equation as $\Delta P = \rho g \Delta h = 36 \text{ kPa}$

2. (10 pts) Using the concept of infinitesimals, show that $dy/dx = e^x$ is the first derivative of $y = e^x$, i.e. that this function is its own derivative, based on the observation that “higher order terms” are negligible. *Hint:* Use the fact that the exponential of any argument β is the series expansion

$$e^\beta = 1 + \beta + \frac{\beta^2}{2!} + \frac{\beta^3}{3!} + \frac{\beta^4}{4!} + \frac{\beta^5}{5!} + \dots$$

Solution: We can think of an (x, y) point on the curve $y = e^x$ and another point very close by, whose coordinates are $(x + dx, y + dy)$. Since the second point is still on this curve, it must also obey $y + dy = e^{x+dx}$. Subtracting y from both sides and making the substitution $y = e^x$, we find

$$dy = e^{x+dx} - e^x = e^x e^{dx} - e^x = e^x (e^{dx} - 1).$$

Now, substitute the series expansion for e^{dx} to obtain

$$dy = e^x \left(1 + dx + \frac{(dx)^2}{2!} + \frac{(dx)^3}{3!} + \frac{(dx)^4}{4!} + \frac{(dx)^5}{5!} + \dots - 1 \right)$$

from which we see that unity cancels and all terms of “higher order smallness” as compared to dx , e.g. those involving $(dx)^2$, $(dx)^3$, etc. can be dropped. What remains is

$$dy = e^x dx \quad \text{which implies} \quad \frac{dy}{dx} = e^x.$$

3. (10 pts) Later we will study the concept of drag force on a vehicle, F_D , for which we’ll develop a general expression of the form

$$F_D = \frac{\rho u^2 A C_D}{2},$$

where ρ is fluid density, u and A are characteristic vehicular velocity and area, respectively, and C_D is a shape-dependent parameter. Infer the physical units of C_D .

Solution: The left-hand side of the equation is a force, for which the units are Newtons, or more basically in the SI system

$$\frac{\text{kg} \cdot \text{m}}{\text{sec}^2}$$

while for the right-hand side, we might write an expression like

$$\underbrace{\frac{\text{kg}}{\text{m}^3}}_{\rho} \cdot \underbrace{\frac{\text{m}^2}{\text{sec}^2}}_{u^2} \cdot \underbrace{\frac{\text{m}^2}{A}} \cdot \underbrace{\text{kg}^a \text{m}^b \text{sec}^c}_{C_D},$$

where a , b , and c are to be determined such that units match-up properly. However, upon inspection, it appears that the product $\rho u^2 A$ already has units of force, leaving us to conclude that C_D is unitless, i.e. $a = b = c = 0$.

4. (10 pts) Fig. 1 shows a conceptually straightforward way of measuring the viscosity, μ , of a Newtonian fluid. Two parallel plates are separated by $h = 0.001 \text{ m}$. The bottom one is fixed, while the top is pulled in-plane. By making some measurements, you are able to infer a constant applied shear stress of $\tau = 1 \text{ N/m}^2$ in this experiment. If the resulting velocity profile is linear (as depicted in the figure), with the fluid's speeds at $y = 0$ and $y = h$ being $u = 0$ and $u = u_0 = 1 \text{ m/s}$, respectively, determine an expression for μ in terms of τ , u_0 , and h and then substitute values to obtain a numerical estimate of μ .

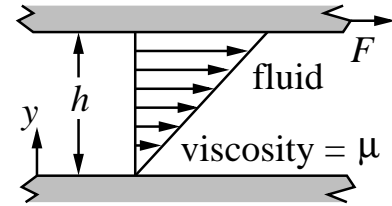


Figure 1: *Simple viscometer.*

Solution: Given that the profile is linear and that the end-conditions are

$$u|_{y=0} = 0 \quad \text{and} \quad u|_{y=h} = u_0,$$

the velocity must be given by the expression

$$u = \frac{u_0}{h} y, \quad \text{whereby} \quad \frac{du}{dy} = \frac{u_0}{h}.$$

Using Newton's Law of Viscosity, we find

$$\tau = \mu \frac{du}{dy} = \mu \frac{u_0}{h}, \quad \text{whereby} \quad \mu = \frac{\tau h}{u_0}.$$

Substituting values, we find

$$\mu = \frac{\tau h}{u_0} = \frac{1 \cdot 0.001}{1} \frac{\frac{\text{N}}{\text{m}^2} \cdot \text{m}}{\frac{\text{m}}{\text{s}}} = 0.001 \frac{\text{N} \cdot \text{s}}{\text{m}^2}.$$

5. (10 pts) The simple viscometer in Question 4 can be realized physically by filling the small gap between 2 concentric cylinders with the fluid, holding the inner cylinder fixed, and rotating the outer cylinder (partial cut-away shown in Fig. 2). If the outer cylinder surface is located at a radius of $R = 0.1 \text{ m}$ and the cylinders have a length of $L = 0.5 \text{ m}$, determine the resisting torque, T , that would be realized for the parameters in Question 4. Neglect any edge effects.

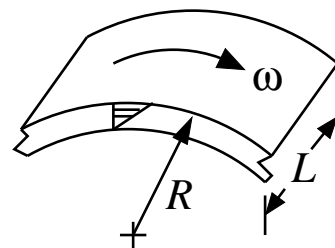


Figure 2: *Cylinders.*

Solution: Question 4 states that the shear stress is constant, so the associated force is simply $F = \tau \cdot A$, where A is the surface area of the rotating cylinder, i.e.

$$A = 2\pi R L = 2 \cdot \pi \cdot 0.1 \cdot 0.5 \approx 0.31416 \text{ m}^2.$$

$$F = \tau \cdot A = 1 \cdot 0.31416 = 0.31416 \text{ N}.$$

Since this acts at right angles at a uniform radius of $R = 0.1 \text{ m}$, the torque is

$$T = F \cdot R = 0.31416 \cdot 0.1 \approx 0.0314 \text{ N} \cdot \text{m} .$$